May 1995

Amplifier

LMC6681

 with

Powerdown Powerdown **Single/LMC6682**

Dual/LMC6684

 Quad Low Voltage,

Rail-To-Rail

 Input and Output CMOS

 \bigotimes National Semiconductor

LMC6681 Single/LMC6682 Dual/LMC6684 Quad Low Voltage, Rail-To-Rail Input and Output CMOS Amplifier with Powerdown

General Description

The LMC6681/2/4 is a high performance operational amplifier which can operate over a wide range of supply voltages, with guaranteed specifications at 1.8V, 2.2V, 3V, 5V, and 10V.

The LMC6681/2/4 provides an input common-mode voltage range that exceeds both supplies. The rail-to-rail output swing of the amplifier assures maximum dynamic signal range. This rail-to-rail performance of the amplifier, combined with its high open-loop voltage gain makes it unique among CMOS rail-to-rail amplifiers. The LMC6681/2/4 is an excellent choice for circuits where the common-mode voltage range is a concern.

The LMC6681/2/4 has a powerdown mode which can be controlled externally. In this powerdown mode, the supply current decreases from 700 µA per amplifier to less than 1 µA per amplifier. The LMC6684 has two powerdown options. Each of the powerdown pins disables two amplifiers.

The LMC6681/2/4 has been designed specifically to improve system performance in low voltage applications. The amplifier's 80 fA input current, 0.5 mV offset voltage, and 82 dB CMRR maintain accuracy in battery-powered systems.

Features

- (Typical unless otherwise noted)
- Guaranteed Specs at 1.8V, 2.2V, 3V, 5V, 10V
- Rail-to-Rail Input Common-Mode Voltage Range
- Rail-to-Rail Output Swing (within 10 mV of supply rail, @ V_S=3V and R_L=10 kΩ)
- Powerdown Mode I_S _{OFF} \leq 1.5 µA/Amplifier (Guaranteed at $V_S = 1.8V$, 2.2V, 3V, and 5V)
- Ultra Low Input Current 80 fA
- \blacksquare High Voltage Gain (V_S = 3V, R_L = 10 kΩ): 120 dB
- Unity Gain Bandwidth 1.2 MHz

- **Applications**
- Battery Operated Circuits
- Sensor Amplifiers
- Portable Communication Devices
- Medical Instrumentation ■ Battery Monitoring Circuits
-
- Level Detectors, Sample-and-Hold Circuits

Ordering Information

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Absolute Maximum Ratings (Note 1)

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 $\Delta \sim 10^{11}$

If Military/Aerospace specified devices are required, please contact the National Semiconductor Sales Office/ Distributors for availability and specifications.

Operating Ratings (Note 1)

3V DC Electrical Characteristics

Unless otherwise specified, all limits guaranteed for T_J = 25°C, V⁺ = 3.0V, V− = 0V, V_{CM} = V_O = V⁺/2, V_{PD} = 0.6V and R_L >
1 MΩ. **Boldface** limits apply at the temperature extremes (Note 16).

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negative slew rates.

Note 9: Input referred, V⁺ = 10V, and R_L = 100 kΩ connected to 5V. Each amp excited in turn with 1 kHz to produce V_O = 2 V_{PP}.

Note 10: V⁺ = 10V. Connected as voltage follower with 8V step Input, and output is measured from 15%-85%. Number specified is the slower of the positive or negative slew rates.

Note 11: Limiting input pin current is only necessary for input voltages that exceed absolute maximum input voltage ratings.

Note 12: Guaranteed limits are dictated by tester limitations and not device performance. Actual performance is reflected in the typical value.

Note 13: CMRR⁺ and CMRR[−] are tested, and the number indicated is the lower of the two values. For CMRR⁺, V⁺/2 < V_{CM} < V⁺ for 1.8V, 2.2V, 3V, 5V, and 10V. For CMRR⁻, 0 < V_{CM} < V⁺/2 for 3V, 5V and 10V. For 1.8V and 2.2V, 0.25 < V_{CM} < V⁺ – 0.3.

Note 14: $V^+ = 10V$, $V_{CM} = 0.5V$. For Sourcing tests, $1V \le V_O \le 5V$. For Sinking tests, $5V \le V_O \le 9V$.

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Note 15: The propogation delays are measured using an input waveform of $f = 5$ Hz, and magnitude of 2.4V. Refer to Section 6.3 and Figures 14, 15 for a detailed explanation.

Note 16: The V_{PD} (threshold low and threshold high) limits are guaranteed at room temperature and at temperature extremes. Room temperature limits are production tested. Limits at temperature extremes are guaranteed via correlation using temperature regression analysis methods. Refer to Section 6.2 for an overview of the threshold voltages.

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Application Information

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1.0 Input Common-Mode Voltage Range

The LMC6681/2/4 has a rail-to-rail input common-mode voltage range. Figure 1 shows an input voltage exceeding both supplies with no resulting phase inversion on the output.

FIGURE 1. An Input Signal Exceeds the LMC6681/2/4 Power Supply Voltages with No Output Phase Inversion

The absolute maximum input voltage at $V^+ = 3V$ is 300 mV beyond either supply rail at room temperature. Voltages greatly exceeding this absolute maximum rating, as in Figure 2, can cause excessive current to flow in or out of the input pins, possibly affecting reliability. The input current can be externally limited to ±5 mA, with an input resistor, as shown in Figure 3.

FIGURE 2. A ±7.5V Input Signal Greatly Exceeds the 3V Supply in Figure 3**, Causing No Phase Inversion Due to RI**

FIGURE 3. Input Current Protection for Voltages Exceeding the Supply Voltage

2.0 Rail-to-Rail Output

The approximated output resistance of the LMC6681/2/4 is 50Ω sourcing, and 50Ω sinking at $V_S = 3V$. The maximum output swing can be estimated as a function of load using the calculated output resistance.

3.0 Low Voltage Operation

The LMC6682 operates at supply voltages of 2.2V and 1.8V. These voltages represent the End of Discharge voltages of several popular batteries. The amplifier can operate from 1 Lead-Acid or Lithium Ion battery, or 2NiMH, NiCd, or Carbon-Zinc batteries. Nominal and End of Discharge of Voltage of several batteries are listed below.

At V_s = 2.2V, the LMC6681/2/4 has a rail-to-rail input common-mode voltage range. Figure ⁴ shows an input voltage extending to both supplies and the resulting output.

FIGURE 4. The Input Common-Mode Voltage Range Extends to Both Supplies at $V_s = 2.2V$

The amplifier is operational at $V_S = 1.8V$, with guaranteed input common-mode voltage range, output swing, and CMRR specs. Figure ⁵ shows the response of the LMC6681/2/4 at $V_S = 1.8V$.

3.0 Low Voltage Operation (Continued)

Figure 6 shows an input voltage exceeding both supplies with no resulting phase inversion on the output.

FIGURE 6. An Input Voltage Signal Exceeds LMC6681/2/4 Power Supply Voltages of V_S = 1.8V with No Output Phase Inversion

4.0 Capacitive Load Tolerance

The LMC6681/2/4 can typically drive a 100 pF load with V_S = 10V at unity gain without oscillating. The unity gain follower is the most sensitive configuration to capacitive load. Direct capacitive loading reduces the phase margin of op-amps. The combination of the op-amp's output impedance and the capacitive load induces phase lag. This results in either an underdamped pulse response or oscillation.

Capacitive load compensation can be accomplished using resistive isolation as shown in Figure ⁷. If there is a resistive component of the load in parallel to the capacitive component, the isolation resistor and the resistive load create a voltage divider at the output. This introduces a DC error at the output.

Figure 8 displays the pulse response of the LMC6681 circuit in Figure ⁷.

FIGURE 8. Pulse Response of the LMC6681 Circuit in Figure ⁷

Another circuit, shown in Figure 9, is also used to indirectly drive capacitive loads. This circuit is an improvement to the circuit shown Figure ⁷ because it provides DC accuracy as well as AC stability. R1 and C1 serve to counteract the loss of phase margin by feeding the high frequency component of the output signal back to the amplifiers inverting input, thereby preserving phase margin in the overall feedback loop. The values of R1 and C1 should be experimentally determined by the system designer for the desired pulse response. Increased capacitive drive is possible by increasing the value of the capacitor in the feedback loop.

4.0 Capacitive Load Tolerance (Continued) The pulse response of the circuit shown in Figure 9 is shown in Figure 10.

Application Hints

5.0 Printed-Circuit-Board Layout for High-Impedance Work

It is generally recognized that any circuit which must operate with less than 1000 pA of leakage current requires special layout of the PC board. When one wishes to take advantage of the ultra-low input current of the LMC6681/2/4, typically less than 80 fA, it is essential to have an excellent layout. Fortunately, the techniques of obtaining low leakages are quite simple. First, the user must not ignore the surface leakage of the PC board, even though it may sometimes appear acceptably low, because under conditions of high humidity or dust or contamination, the surface leakage will be appreciable.

To minimize the effect of any surface leakage, lay out a ring of foil completely surrounding the LMC6681/2/4's inputs and the terminals of capacitors, diodes, conductors, resistors, relay terminals, etc. connected to the op-amp's inputs, as in Figure ¹¹. To have a significant effect, guard rings should be placed in both the top and bottom of the PC board. This PC foil must then be connected to a voltage which is at the same voltage as the amplifier inputs, since no leakage current can flow between two points at the same potential. For example, a PC board trace-to-pad resistance of 1012Ω, which is normally considered a very large resistance, could leak 5 pA if the trace were a 5V bus adjacent to the pad of the input. This would cause a 60 times degradation from the LMC6681/2/ 4's actual performance. However, if a guard ring is held within 5 mV of the inputs, then even a resistance of 10^{11} Ω would cause only 0.05 pA of leakage current. See Figure ¹² for typical connections of guard rings for standard op-amp configurations.

FIGURE 12. Typical Connections of Guard Rings

The designer should be aware that when it is inappropriate to lay out a PC board for the sake of just a few circuits, there is another technique which is even better than a guard ring on a PC board: Don't insert the amplifier's input pin into the board at all, but bend it up in the air and use only air as an insulator. Air is an excellent insulator. In this case you may have to forego some of the advantages of PC board construction, but the advantages are sometimes well worth the effort of using point-to-point up-in-the-air wiring. See Figure 13.

6.0 Powerdown

6.1 PINOUT FOR THE LMC6681/LMC6682/LMC6684

For the LMC6681/2/4, the input, output, and power pins are the same as those used in the standard configuration. One of the other pins, pin 5 in the case of the LMC6681, is used to enable the powerdown mode. The connection diagrams for the LMC6681/2/4 are on the front page of the datasheet. The LMC6684 has 2 powerdown options. Each of the powerdown pins disables two amplifiers. If both the powerdown pins are pulled high, all four amplifiers will be disabled. Referring to the connection diagrams on the front page of the datasheet, Pin 5 disables amplifiers B and C and Pin 13 disables amplifiers A and D.

6.2 EXPLANATION OF DATASHEET PARAMETERS

The LMC6681/2/4 is ON (meets all the datasheet specs) when the voltage applied to the powerdown pin, V_{PD} is a logic low. The device is OFF when V_{PD} is a logic high. These logic levels are indicated in the test conditions in the datasheet tables. Summarizing these numbers:

In applications where the powerdown pin is not connected externally, it is pulled to a logic low internally through a current source. The t_{ON} and t_{OFF} specs will essentially be the same for a V_{PD} in the specified range. This means that the LMC6681/2/4 will typically be fully operational 50 us after a logic low has been applied to the powerdown pin. Please note that the frequency of V_{PD} in the test circuit below is 5 Hz.

6.0 Powerdown (Continued)

6.3 TEST CIRCUIT TO MEASURE t_{ON} **AND** t_{OFF}

The circuit used to measure the t_{ON} , and t_{OFF} during the powerdown operation is a voltage follower with a load of 2 k Ω as shown in Figure 14.

When the input to the powerdown pin is low, the LMC6681/ 2/4 is on. Since the amplifier is connected in the voltage follower configuation, the output of the circuit is −1V. When the

powerdown pin is pulled high, the amplifier shuts down, and draws less than 1 µA/Amplifier. In this powerdown mode, the output pin has high impedance, and the output of the circuit is pulled to 0V. t_{ON} is specified as the time between the 50% points of the trailing edges of the input waveform at the powerdown pin, and the waveform at the output pin. Similarly, the t_{OFF} is specified as the time between the 50% points of the leading edges of the input waveform at the powerdown pin, and the waveform at the output pin.

The t_{ON} (time delay for device to power on) the t_{OFF} (time delay for device to power off) specs are guaranteed at a supply voltage of 3V. The t_{ON} and t_{OFF} spec are independent of the V_{PD} applied in the specified range. Refer to the Powerdown DC Threshold Characteristics table for the values for a logic low and a logic high.

The guaranteed spec for t_{ON} is 200 µs. This does not mean that the signal to the V_{PD} pin can be as high as 5 kHz (1/200) μ s). Note that the V_{PD} frequency for the t_{ON} and t_{OFF} measurements is 5 Hz. The LMC6681/2/4 is ideal for DC type applications where the powerdown pin is controlled by low frequency signals.

When the LMC6681/2/4 is powered off, internal bias currents are shutoff. There is a inherent latency in the circuit, and the device has to power off for a certain period of time for the t_{ON} spec to apply. Refer to the figure below. $t_{PD OFF}$ refers to the time interval for which the device is in the powerdown mode. Consider the case when the device has been powered off for 5 ms, and then the powerdown pin is pulled to a logic low. From Figure 16, at room temperature, the device powers on after 500 µs.

 t_{PDOFF} in Powerdown Mode, $V_{\text{S}} = 3V$

7.0 Compensating for Input Capacitance

It is quite common to use large values of feedback resistance with amplifiers that have ultra-low input current, like the LMC6681/2/4. Large feedback resistors can react with small values of input capacitance due to transducers, photodiodes, and circuits board parasitics to reduce phase margins.

FIGURE 17. Canceling the Effect of Input Capacitance

The effect of input capacitance can be compensated for by adding a feedback capacitor. The feedback capacitor (as in Figure 17), C_F , is first estimated by:

$$
\frac{1}{2\pi R_1 C_{\text{IN}}}\geq \frac{1}{2\pi R_2 C_F}
$$

or

$$
R_1 C_{IN} \leq R_2 C_F
$$

which typically provides significant overcompensation.

Printed circuit board stray capacitance may be larger or smaller than that of a breadboard, so the actual optimum value for C_F may be different. The values of C_F should be checked on the actual circuit. (Refer to the LMC660 quad CMOS amplifier data sheet for a more detailed discussion.)

8.0 Spice Macromodel

A Spice Macromodel is available for the LMC6681/2/4. The model includes a simulation of:

- Input common-mode voltage range
- Frequency and transient response
- GBW dependence on loading conditions
- Quiescent and dynamic supply current
- Output swing dependence on loading conditions

and many more characteristics as listed on the macromodel disk.

Contact the National Semiconductor Customer Response Center at 1-800-272-9959 to obtain an operational amplifier spice macromodel library disk.

Applications

Transducer Interface Circuits

A. PIEZOELECTRIC TRANSDUCERS

FIGURE 18. Transducer Interface Application

The LMC6681 can be used for processing of transducer signals as shown in the circuit below. The two 11 MΩ resistors provide a path for the DC currents to ground. Since the resistors are bootstrapped to the output, the AC input resistance of the LMC6681 is much higher.

FIGURE 19. LMC6681 Used for Signal Processing

An input current of 80 fA and a CMRR of 82 dB causes an insignificant error offset voltage at the output. The rail-to-rail performance of the amplifier also provides the maximum dynamic range for the transducer signals.

B. PHOTODIODE AMPLIFIERS

FIGURE 20. Photodiode Amplifier

Photocells can be used in light measuring instruments. An error offset voltage is produced at the output due to the input current and the offset voltage of the amplifier. The LMC6682, which can be operated off a single battery is an excellent choice for this application with its 80 fA input current and 0.5 mV offset voltage.

FIGURE 21. Low Voltage Peak Detector

The accuracy of the peak detector is dependent on the leakage currents of the diodes and the capacitors, and the non-idealities of the amplifier. The parameters of the amplifier which can limit the performance of this circuit are (a) Finite slew rate, (b) Input current, and (c) Maximum output current of the amplifier.

The input current of the amplifier causes a slow discharge of the capacitor. This phenomenon is called "drooping". The LMC6682 has a typical input current of 80 fA. This would cause the capacitor to droop at a rate of $dV/dt = I_B/C$ = 80 fA/100 pF = 0.8 mV/s. Accuracy in the amplitude measurement is also maintained by an offset voltage of 0.5 mV, and an open-loop gain of 120 dB.

Oscillators

FIGURE 22. 1 Hz Square — Wave Oscillator

For single supply 5V operation, the output of the circuit will swing from 0V to 5V. The voltage divider set up R_2 , R_3 and $R₄$ will cause the non-inverting input of the LMC6681/2/4 to move from 1.67V (1/3 of 5V) to 3.33V (2/3 of 5V). This voltage behaves as the threshold voltage.

 R_1 and C_1 determine the time constant for the circuit. The frequency of oscillation, $f_{\rm OSC}$ is

$$
\left(\frac{1}{2\Delta t}\right)
$$

where ∆t is the time the amplifier input takes to move from 1.67V to 3.33V. The calculations are shown below.

$$
1.67 = 5\left(1-e^{-\frac{t_1}{\tau}}\right)
$$

where τ = RC = 0.68 seconds

 \rightarrow t₁ = 0.27 seconds.

and

$$
3.33 = 5\left(1 - e^{-\frac{t_2}{\tau}}\right)
$$

 $\rightarrow t_2$ = 0.74 seconds Then,

$$
f_{\text{OSC}} = \left(\frac{1}{2\Delta t}\right)
$$

$$
= \frac{1}{2(0.74 - 0.27)}
$$

$$
\frac{2(0.74-0.27)}{1 \text{ Hz}}
$$

LMC6681/2/4 as a Comparator

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Figure 23 shows the application of the LMC6681/2/4 as a comparator. The hysteresis is determined by the ratio of the two resistors. Since the supply current of the LMC6681/2/4 is less than 1 mA, it can be used as a low power comparator, in applications where the quiescent current is an important parameter. At $V_s = 3V$, typical propagation delays would be on

the order of $t_{PHL} = 6 \mu s$, and $t_{PLH} = 5 \mu s$.

Filters

FIGURE 24. Wide-Band Band-Pass Filter

The filter shown in Figure 24 is used to process "voice-band" signals. The bandpass filter has a gain of 40 dB. The two corner frequencies, f_1 and f_2 are calculated as

$$
f_1 = \frac{1}{2\pi R_1 C_1} = \frac{1}{2\pi (10 \text{ k}\Omega) (79 \text{ nF})} = 200 \text{ Hz}
$$

$$
f_2 = \frac{1}{2\pi R_2 C_2} = \frac{1}{2\pi (1 \text{ M}\Omega)(40 \text{ pF})} = 4 \text{ kHz}
$$

Filters (Continued)

The LMC6681/2/4, with its rail-to-rail input common-mode voltage range and high gain (120 dB typical, $R_L = 10 kΩ$) is extremely well suited for such filter applications. The rail-to-rail input range allows for large input signals to be processed without distortion. The high gain means that the circuit can provide filtering and gain in one stage, instead of the typical two stage filter. This implies a reduction in cost, and savings of space and power.

This is an illustration of the conceptual use of the LMC6681/ 2/4. The selectivity of the filter can be improved by increasing the order (number of poles) of the design.

Sample-and-Hold Circuits

FIGURE 25. Sample-and-Hold Application

When the "Switch" is closed during the Sample Interval, C_{HOLD} charges up to the value of the input signal when the "Switch" is open, C_{HOLD} retains this value as it is buffered by the high input impedance of the LMC6681.

Errors in the "hold" voltage are caused by the input current of the amplifier, the leakage current of the CD4066, and the leakage current of the capacitor. While an input current of 80 fA minimizes the accumulation rate for error in this circuit, the LMC6681's CMRR of 82 dB allows excellent accuracy throughout the amplifier's rail-to-rail dynamic capture range.

FIGURE 26. Circuit Used to Sense Charging

FIGURE 27. Circuit Used to Sense Discharging

The LMC6681/2/4 has been optimized for performance at 3V, and also has guaranteed specs at 1.8V and 2.2V. In portable applications, the R_{LOAD} represents the laptop/
notebook, or any other computer which the battery is powering. A desired output voltage can be achieved by manipulating the ratios of the feedback resistors. During the charging cycle, the current flows out of the battery as shown. While during discharge, the current is in the reverse direction. Since the current can range from a few milliamperes to amperes, the amplifier will have to sense a signal below ground during the discharge cycle. At 3V, the LMC6681/2/4 can accept a signal up to 300 mV below ground. The common-mode voltage range of the LMC6681/2/4, which extends beyond both rails, is thus a very useful feature in this application.

A typical offset voltage of 0.5 mV, and CMRR of 82 dB maintain accuracy in the circuit output, while the rail-to-rail output performance allows for a maximum signal range.

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Notes

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